EXHIBIT "A"

ELECTRO-OPTICAL CABLE FOR USE IN TRANSMISSION OF HIGH VOLTAGE AND OPTICAL SIGNALS UNDER EXTREMES OF TEMPERATURE AND ALTITUDE

Statement of Government Interest

The invention described herein was made under Contract No. N0019-96-C005 with the Government of the United States of America and may be manufactured and used by and for the Government of the United States of America for Governmental purposes without the payment of any royalties thereon or therefor.

Background of the Invention

1. Field of the Invention

The present invention relates to towed decoys for use in aviation, and more particularly to electro-optical cables for use in such towed decoys.

2. Brief Description of Prior Developments

It is known in the art to provide a decoy which is towed on an electro-optical cable from a combat aircraft. While such arrangements have generally performed well, there is a need to still further improve the temperature, mechanical, electrical and environmental durability of such electro-optical cables.

Summary of Invention

The present invention is an electro-optical signal cable which has improved the temperature, mechanical, electrical, and environmental durability. Volumetric and weight impacts are minimized, thus significantly extending applicability beyond current existing design limitations.

Improved durability has been achieved by acknowledging the three distinct elements of the cable and addressing each separately then merging the elements into a single design. The constituent layers are combined in a synergistic manner. electrical conductors make use of adhesive materials in order to fuse the dielectric materials to the wire. The resulting wire construction method demonstrates excellent dielectric withholding potential, over 5 kV, at temperatures of up to 700 degrees Fahrenheit. The fiber optic element has been improved through consideration of the optical fiber as a portion of a composite beam, in which the fiber was encased in a cushion of PTFE, Polytetrafluorethylene, TEFLON, then a thermo-plastic resin, PEEK, Polyetheretherketone, was utilized to provide a tough, hard, outer shell which improved both thermal and mechanical durability to levels in excess of 700 degrees Fahrenheit. The electrical conductors have layers of dielectric PTFE and aromatic co-polyimides such as BPDA-PDA and PMDA-ODA. The conductors are copper with a plating of a diffusion barrier such as nickel. The braid selected consisted of a PBO, Poly(pphenylene-2,6-benzobisoxazole), Zylon, outer jacket with a friction reducing coating included to aid in deployment of the material. The resulting cable system has proven performance when subjected to the rigors of the after-burning plume of a jet engine installed in the Navy's F/A-18E/F fighter aircraft. Research performed in the conduct of the development of the advanced durability cable has lead to the potential for further increases to thermal and mechanical performance through the use of advanced polymers such as Upilex-S and other co-polymers based on aromatic polyimides such as BPDA-PDA and PMA-ODA and films made of PBO, basic material only testing indicates a

further enhancement in performance. The application method would be the same as that for the cable claimed herein, thus is a further claim of this patent disclosure.

Brief Description of the Drawings

The present invention is further described with reference to the accompanying drawings, wherein:

Figure 1 is a vertical cross sectional view of the electro-optical cable of the present invention.

Detailed Description of the Preferred Embodiment

A preferred embodiment of the present invention is described with reference to Figure 1 and Table 1. The reference numbers on Figure 1 are identified on Table 1.

	Signal-Con	ductors
	Baseline	Upgrade
1	32 Ga Copper	PTFE
2	MIL-ENE 0.002"/0.003"	PTFE 0.0005"
3	·	EKJ
	N/A	0.003"
		0.004"
		0.006"

	Signal-C	ptics
	Baseline	Upgrade
4	Glass	Glass
5	Acrylate 245 microns	Polymide 152 microns
6	PTFE 0.003"	PTFE 0.003"
7	FEP 600 micron OD	PFA and PEEK 600 micron OD

Table 1

A further disclosure and a preferred embodiment and tests showing surprising and unexpected results are shown in the following attached exhibits:

Exhibit "A" Tow/Signal Line Development

Exhibit "B" Phase C Thermal Upgrade Towline Flight Test Review

Exhibit "C" Past Flight Tow/Signal Line Analysis

It will be appreciated that an electro-optical cable has been described which is durable under adverse temperature, mechanical, electrical and other environmental conditions.

While the present invention has been described in connection with the preferred embodiments of the various figures, it is to be understood that other similar embodiments may be used or modifications and additions may be made to the described embodiment for performing the same function of the present invention without deviating therefrom. Therefore, the present invention should not be limited to any single embodiment, but rather construed in breadth and scope in accordance with the recitation of the appended claims.

Claims

What is claimed is:

1. An electro-optical cable comprising:

an optical element comprising an elongated glass fiber core, a medial cushioning layer concentrically surrounding the glass fiber core, and an outer hard shell material surrounding the medial cushioning layer; and

at least one electrically conductive element comprising an elongated conductive core and a dielectric layer concentrically surrounding the electrically conductive element.

- 2. The electro-optical cable of claim 1 wherein the medial cushioning layer of the optical element comprises polytetrafluorethylene.
- 3. The electro-optical cable of claim 1 wherein the outer hard shell layer of the optical element comprises polyetheretherketone.
- 4. The electro-optical cable of claim 1 wherein the conductive core of the electrically conductive element comprises copper.
- 5. The electro-optical cable of claim 1 wherein the dielectric layer of the electrically conductive element comprises dielectric polytetrafluorethylene.
- 6. The electro-optical cable of claim 1 wherein the electrically conductive element has a layer of an aromatic co-polyimide concentrically surrounding the dielectric layer.

7. The electro-optical cable of claim 1 the wherein optical element has a layer selected from an acylate and a polymide interposed between the glass core and the cushioning layer.

Abstract

An electro-optical cable comprising an optical element comprising an elongated glass fiber core, a medial cushioning layer concentrically surrounding the glass fiber core, and an outer hard shell material surrounding the medial cushioning layer; and at least one electrically conductive element comprising an elongated conductive core and a dielectric layer concentrically surrounding the electrically conductive element.

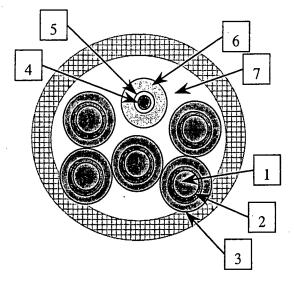


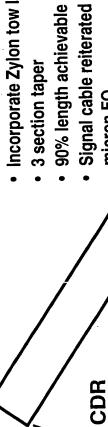
Figure 1



Line Development Dr. John Dion



Baseline Tow/Signal Line Development History



- Incorporate Zylon tow line
- Signal cable reiterated to 600 micron FO

Technora selected over Kevlar

86% tow length achieved

Driven by strength margin

requirements/volume

Strength optimized vs.

Signal cable selection

length

Technora jacket

Tapered cable (2 section)

- Iterated tow line to 2-section Eliminate termination/bury issues taper
- 85% length achievable
- Government acceptance of 85%
- Signal cable iterated
- Zylon jacket

- Three section taper tow line
 - Optimize length
- Identified Zylon (PBO) as candidate material

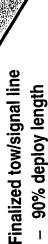
5 - 32 AWG conductors

250 micron FO cable

No rotary joints

- ~1.5X strength of Technora
- IRAD program funded to characterize
- Finalized tow/signal line
- HM Zylon w/fiberline lubrication

achievable





Baseline Cable Design

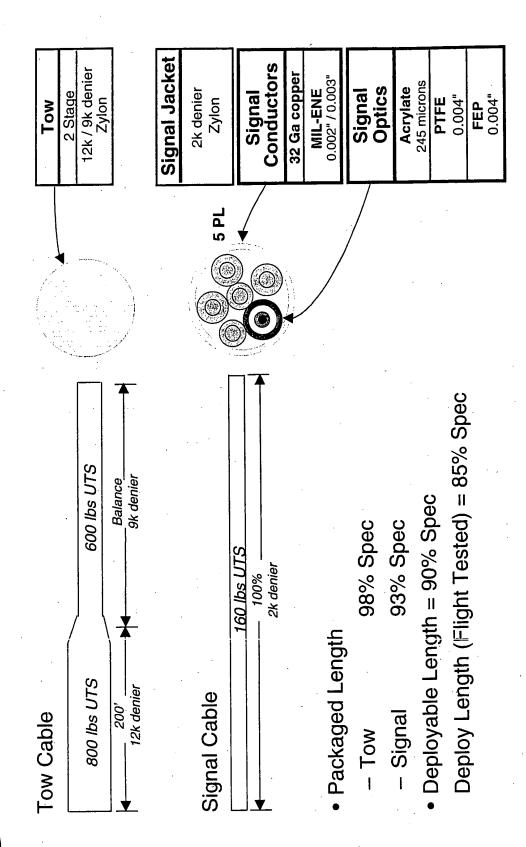
- Towline
- Zylon-HM
- High modulus, reduce strain @ load
- Reduce load transmitted to wrapped signal cable
- Two segment taper
- 0.040", 0.052" diameter (600 and 900 lb strength)
- Better than 150% strength margin (1.9)
- Fiberline friction reducing coating applied (sizing of fibers) produces significant improvements in terms of abrasion resistance

Signal Line

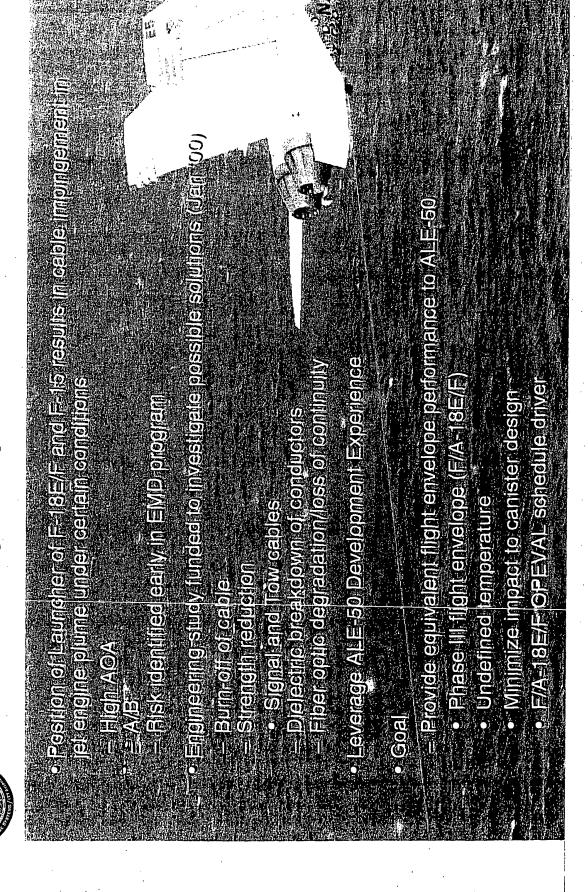
- Zylon-HM
- 5 x 32 AWG Cu conductors and 600 micron FO
 - 0.045" diameter (160 lb strength)
- Better than 200% strength margin (2.8)
- Fiber Optic safety factors >200% UTS data
- Fiberline friction reducing coating

Baseline (Standard) Tow/Signal Cable





Reason for High Temperature Cable





Towline Thermal Upgrade Program

- Three phase development plan established to upgrade IDECM Cables
- F/A-18E/F installation requires thermally ruggedized tow/signal line
- Objective is to meet/exceed Phase III envelope established for F/A-18E/F OPEVAL
- Phase 0 characterization effort
- Baseline ALE-55 vs. ALE-50 cable comparison test complete
- Performance drivers are strength and HV hold-off at elevated temperature

Phase 1 Lab development effort (Jun 00)

- Cable/material development
- Strength member, HV conductors and FO
- Development focus on available materials (organic/inorganic polymers)
- -- Candidates identified and in test
- HV mass model feasibility evaluation
- Evaluation of system/FOTD round impacts
- Line length, multiple deploy lengths
- Phase 2 Flight development effort (Nov 00)
- Material characterization
- Canister implementation
- Assets available for initial flight testing



Baseline Cable Plume Damage



• F/A-18E/F Fast Deploy Test

 Plume induced heat damage during low AOA A/B maneuver – 2 seconds plume impingement

MILENE melted -> wire shorting

 Laboratory testing shows milene melting begins @ 300°C Fiber coatings flowed -> loss of optical continuity

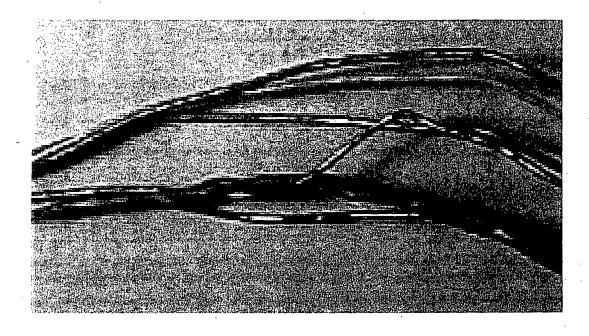


Baseline Cable Plume Damage

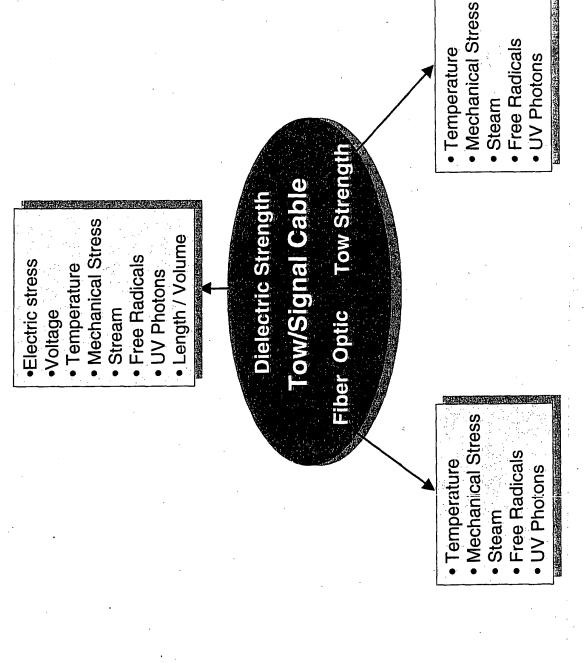
F-15 Safe Separation Flights (Phase 3A)

Plume induced A/B heat damage

- MILENE softened which resulted in shorting
 Fiber coatings flowed causing loss of optical continuity



Materials/Effects for Plume Endurance



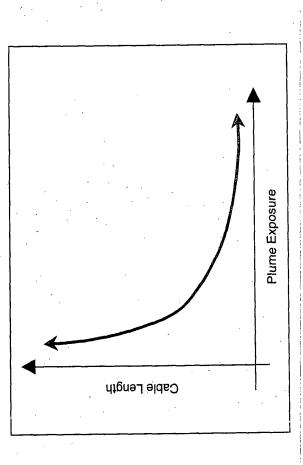




The Optimization Problem

Maximizing cable length consists of minimizing:

- Dielectric coating
- Fiber optic coatingZylon signal jacket thicknessZylon tow diameter
- Maximizing plume exposure would minimize length



Dielectric (Conductor Insulation) Candidates



Extensive literature search, vendor correspondence, and consultant involvement

Parallel study efforts (MIT/EWAT & NRL)

- GE Corporate Research and Development

Options Evaluated/Tested

Ceramics

- Glasses

HybridsTeflon

Kapton Variations



Selected Test Results (Dielectric)

 Based on BAE SYSTEMS electrode testing (10 min, no load) Polymer Dielectric Performance (Top Tier Candidates)

	Dielectr	ic Breakdo	wn Voltage	Dielectric Breakdown Voltage @ temp (KV/mil)	KV/mil)	5KV / 500 °C
Film (polymer)	3.00E	400 °C	2. 00s	2:0 °C	600 °C	Insulation Required (mils)
Teflon (PTFE)	0.8	0.65	0.45*	N/A	N/A	11.0
Kanton H (PMDA-ODA)	3.0	2.0	0.71	0.025*	N/A	7.0
Kapton E (BPDA-PDA/PDMA-CDA)	2.0	1.1	0.75	0.625*	N/A	6.7
Upilex-S (BPDA-PDA)	2.0	1.5	0.95	0.7	0.43*	5.0

^{*} Temperature onset for brittleness / high shrinkage / degradation

EXHIBIT "B"

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Phase C Thermal Upgrade Towline Flight Test Review



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Agenda

Conclusions/Recommendations



Objectives

- Review Towline Phase C Test Results
- Review Findings
- Discuss Recommendations Going Forward



Program Background

- Thermal Upgrade Not Part of EMD Contract
- Navy Recognized Need to Pursue Enhancement
- Funded Off Contract Effort
- Specific to F-18E/F Aircraft

Engineering Study

- Evaluate Materials for High Temperature Use
- ✓ FO Coatings
- ✓ Dielectric Material
- ✓ Strength Members
- Perform Laboratory Testing
- Select Candidate Tow/Signal Line Configurations
- Conduct Flight Tests
- Down Select To Final Configuration
- Support Proof of Concept Flight Tests

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Executive Summary

Highlights

- Demonstrated Excellent Thermal Performance
- No Thermally Induced Failures Within Goal Envelope
- Eliminated FO Failures During Deployment
- Demonstrated Excellent System Performance During Mission/Combat Representative Maneuvering
- Verified ALL Corrective Actions Implemented From Previous Phases
- ✓ BAE Snubber vs. Greene Rubber Snubber
- ✓ Brake Assembly Acceptance Criteria

Challenges Remaining

- "No Hit" Separation
- Resolution to "High Twist" Mechanical Failures

Canister Configuration

B. Sarantis

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Canister Configuration Summary

Phase C Mass Model Round P/N 6273250G6

Similar to Baseline Mass Model Round Except:

· Utilizes High Voltage Mass Model

- Thermally Upgrade Tow and Signal Line

Teflon Impregnated Rounded Fins Upgraded Fin Damper Mechanism

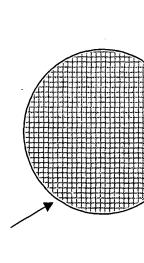
✓ 275 msec Time Delay

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Tow/Signal Line Configuration

0.072" @ 24k Denier





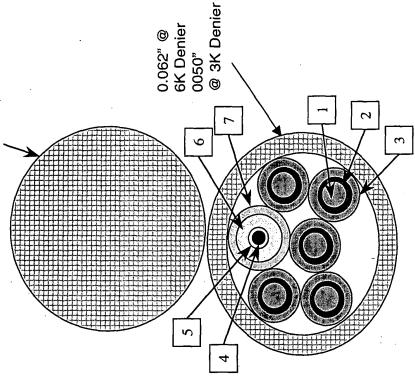
0.045"

	_	_	_	8.6579		_
Upgrade	3 Stage	24k / 12k / 9k	denier	Signal - Jacket	Upgrade	6k / 3k denier
Baseline	2 Stage		12k / 9k denier	Signal	Baseline	2k denier

	•	•	•	0.062" @	6K Denie

	Signal - Co	Conductors
	Baseline	Upgrade
1	32 Ga copper	32 Ga copper
	MIL-ENE	PTFE
2	0.002" / 0.003"	0.0005"
		CXE
3	N/A	0.004"

-	32 Ga copper	32 Ga copper
	MIL-ENE	PTFE
2	0.002" / 0.003"	0.0005"
		EKJ
3	N/A	0.004"
H		
	Signal -	Optics
1	Baseline	Upgrade
4	Glass	Glass
	Acrylate	Polyimide
2	245 microns	152 microns
	PTFE	PTFE
9	0.003"	0.003"
	d 3 4	PEEK
7	600 micron OD	600 micron OD



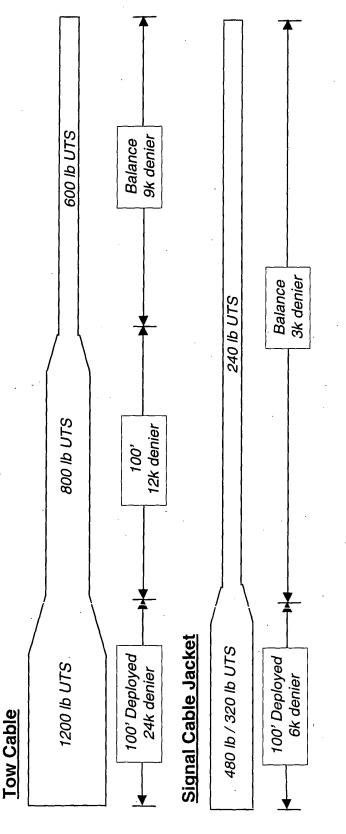
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Baseline Cable System



Tow/Signal Line Configuration

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Packaged length

- Tow 72% (vs original spec)
- Signal 60% (vs original spec)
- Deploy Length = 58% (vs original spec)

Worst Case Margin (@ 58%)

- Tow: 3.3
- Signal: 3.6

✓ Glass better than 2.0

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Flight Test Report

D. Davidson

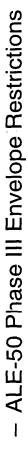
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Evaluate Selected Tow/Signal Line Throughout F/A-18E/F Flight Envelope

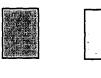


Evaluate Overall Canister / Round Performance

- Launch, Deploy, Continuity and Tow

Evaluate Safe Separation Performance

- F/A-18E/F



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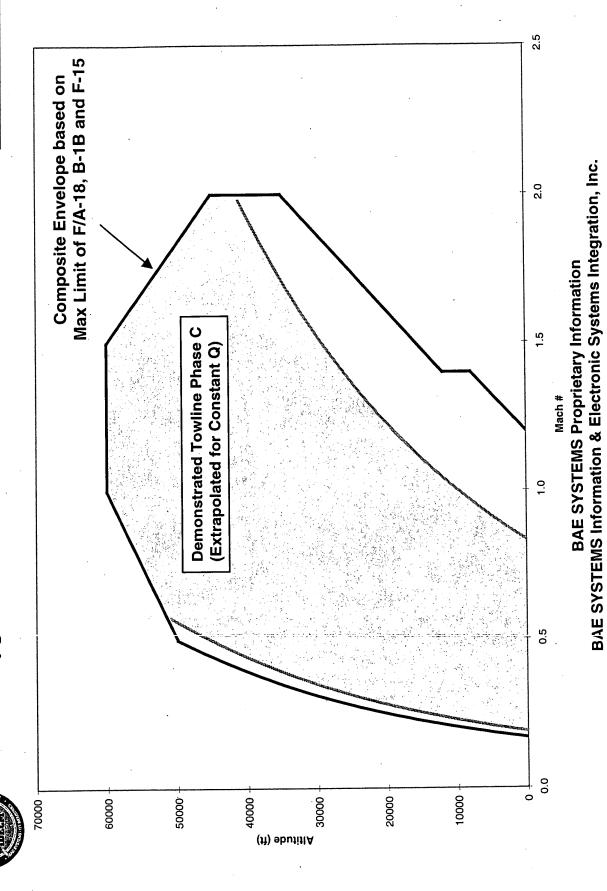
Flight Test Configuration

- Platform
- F/A-18 F2 (Flights 1-3)– F/A-18 E5 (Flights 4-10)
- High Speed Cameras
- Conventional Installation
- **Center Line Tank Included** For Some Deployments

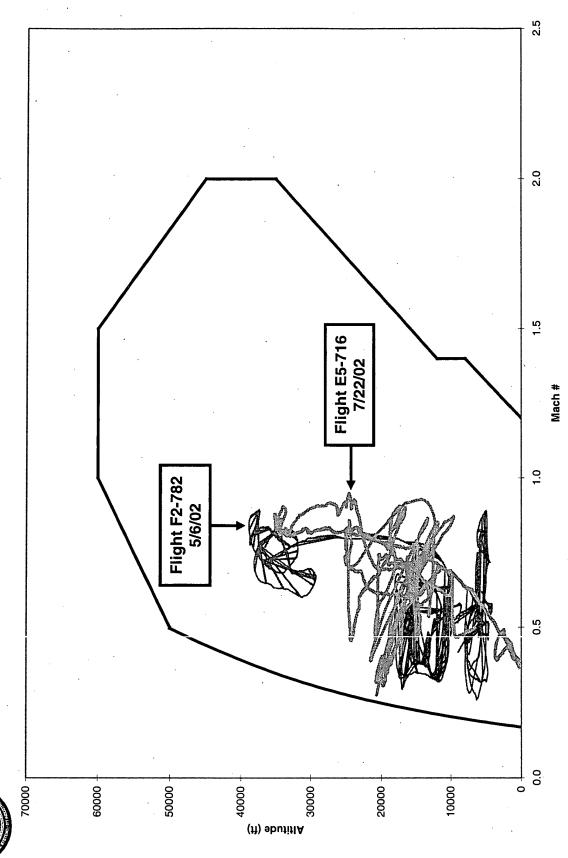
- **System Components**
- RFCM
- IMPLC
- BCC
- ✓ SW Version 2.3.B.B
- ⇒ 58% Deployment Length T-3F Launcher
- ✓ Fuselage Installation

 - HVS Box
- **Production Towline Extension**

Thermal Upgrade Canister Demonstrated Flight Envelope



Representative Flight Test Profiles



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Phase C Demonstrated Maneuver Highlights

MAX A/B AOA Highlights

$$-7^{\circ} \ge 35K$$

MIL Power Highlights

Combat Maneuvers

- Aileron Roll
 - Lag Roll
- High Yo Yo Extension/Pitchback
- Maximum Performance Break Turn
- Pushover from Horizontal Scissors
 - Squirrel Cage
- Simulated Bomb Run



Phase C Flight Test Summary

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ł			9/4			Safe	1111	Stable	Continuity	uity		å		Max /	Max A/B AOA Achieved	A Achie	pave		
	Date	Alt (Ft)	(KCAS)	Q (psf)	Eject	Separation	Deploy	_	Electrical	50	Strength	Time	A/B Exp	똤	15K	25K	35K	Comments	
I -		10,500	325	348	X 0	λ.	λ	Ą	59 Min	56 Min	To Sever (64 Min)	56 Min	80 Sec	10	3°	N/A	7°		
i .		10,000	375	457	<i>></i> :	Scratch	>	٨	98 Min	96 Min	To Sever (109 Min)	96 Min.	20 Sec	2°.	N/A	N/A	N/A		
		10,000	425	604	۶	Scratch	X	>	2.5 Min	2.5 Min	To Sever (48 Min)	2.5 Min	10 Sec	10	N/A	N/A	N/A	Attempted High Risk Test Point First	
		10,700	378	449	λ,	Scratch	z	Ϋ́	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	Reel Count Circuit Failure	
		10,100	374	449	$\tilde{\lambda}^{(i)}$	Scratch	Å	λ,	77 Min	62.Min	To Sever (77. Min)	62:Min	42 Sec	ဗိ	A/A	N/A	N/A	LOST FO during 5K, 2° AOA A/B Manuever. Electrical Cont maintained throughout.	
		10,200	374	449	λ	Scratch*	.	Å	68 Min	uiW:89	To Sever (68 Min)	68 Min	29. 39.	A/N	ဗိ	N/A	2	HVS Breakdown prior to 35K test points traced to breakdown in captive carry canister. Entire sytem checked OK post flight.	
		10,000	375	449	<i>*</i>	Scratch*	λ	<u>ا</u> ۲.	9 Min	9 Min »	Broke @ 9 Min	9 Min	N/A	N/A	N/A	A/N	N/A	Decoy broke off during >7g Break Turn	
		10,000	374	449	>	Scratch	λ.,	, A	110 Min	110 Min	To Sever (110 Min)	110 Min	*62 Sec	N/A	N/A	4°	7°	No HVS Data. Entire System Checks OK Post Flight.	
		10,000	375	449	>	Scratch*	λ.	>	47 Min	47 Min	To Sever (64.5 Min)	47 Min	N/A	N/A	N/A	N/A	N/A	Lost FO and HV During Simulated Bomb Run Dive (45° dive, >530 KCAS)	
		10,000	. 375	449	> ,	Scratch*		> 20 > 20 > 30	51 Min	69 Min.	Broke @	51 Min	65 Sec.	N/A	A/A	%	လိ	Exceeded Goal Envelope @ 25K. Subsequently lost HV during 35K, 5° AOA A/B maneuver. Towline Broke during 5K, 3° AOA A/B maneuver.	

* Centerline Tank Installed

	Safe	Full	Stable	Cont	ontinuity		ô	Total	Max /	VB AO	A Achi	eved
Figure	Š	Deploy	Flight	Electrical	6	Strength	Time	A/B Exp	5K	15K	25K	35K
100%	Scratch	%06	100%	89%	89%	89%	56 Min	339 Sec	3°	3°	4۰	٦.,
										I		

Phase C Summary

*ALE-55 Canister Ready For DT/OTI



MAX A/B Survivability Summary

F2-782 F2-783 E5-713 E5-714 E5-716

			The state of the s		_
(FO Only)				7	
(FO Only)			:	9	
				5	
			Street	4	AOA
				3	AC
				2	
				1	
35000	25000	15000	0009	0	
	35000				

ALTITUDE

ALE-55 Canister Achieved Phase C AVB Objectives

Post Flight Hardware Analysis

B. Sarantis





Tear Down Analysis Overview

Conducted Complete Tear Down Analysis on All Canisters, Decoys and Cables Returned from Phase C Flight Tests

No Evidence of Workmanship Problems Found Which Caused Flight Problems No Evidence of Thermally Induced Damage to The FO or Conductors



Hardware Summary

	Hot Zone		2/02 0000		Good FO/C			0,01	2000 rO/C	N/A	Good FO/C		Good FO/C			Good FO/C		Good FO/C		Good FO/C,	A/N				
Cable Info	Standoff	Made	OIG MAIN		Two Marks			0.00	Oliset Marks Good FU/C	N/A	One Mark		One Mark			One Mark		One Mark		One Mark	One Mark				
	Flapper	Journal A	NOTETIAL		Normal			10,10	Normai	N/A	Normal		Normal			Normal		Normai		Normal					
Decoy Info										Lost						Lost 2					l ost 3				
	Brake	Normani	NO.		Normal			No man	Normal	Normal	Normal		Normal			Normal		Normal		Normal	TBD4				
Canister Info	Flapper	Normol .	NO.		Normal			1014	Normal	Normal	Normal		Normal			Normal	-	Normai		Normal	TBD4				
Ö	Snubber	Mormal	Milai		Normal				Norman	Normal	Normal		Normal			Normal		Normal		Normai	TBD4				
A/B Time	_	8	十		20			T	2	N/A	42		09			N/A		29		N/A	65	T	T	1	1
Elect	(Min)	5	S		98			,	6.7	N/A	77		89			6				47	5.1		1	1	
FO	(Min)	8	3		96			,	63	N/A	62		89			6		2		47	69		T	1	
Flight Time	(Min)	2	5		109			ę	9	N/A	77		68			6		219		64.5	69				
AB/Alt	,	251 24567	15K, 2.3	5k,1 fail FO	5K, 1, 2	FO Pre-A/B	HV (Cath) In A/B		3N, 1, rall r0/330V	N/A	5K 3,2,1	Failed FO only @ 2	15K, 2,3	35K 5,6,7		N/A	, , , , ,	25K, 3,4	35K, 3,6,7	N/A	25K 3 4Brkdn	35K F G 7	HV (Cath) @ 5	11V (Call) & 3	5K, 3 LINe Broke
CL Tank		Z	2		Z			Z	2	z	Z		Υ			\		z		>	>				
٥		248			457			700		449	449		449			449	-	443		449	449		I	\rfloor]
KCAS		306	1_		375			425	2	378	374		374			375		3/4		375	375			1	
ALT		10 FK	5		10k			5	5	10.7K	10.1K		10.2K			10Ķ		ş		ş	Ş				
	Plane/Pos	E9 / 3	2 / 3		F2/3			0 / 02	2/2	E5/1	E5 / 1		E5/1			E2/3		E2 /3		E5/3	E5/3				
Snubber		a	5		GR			9	5	GR	BAE		BAE			BAE	1	BAE		BAE	RAF	!!			
S/N		ğ	2		22			6	*7	11	30		33		_	29		8		34	28				

Reel Count Failure. Signal line was completely unwound and pulled off signal spindle.
 Decoy lost during maximum perfromance break turn (7 g.)
 Line broke during 5K, 3° AOA, Max A/B turn
 Canister inspection not completed. Awaiting return of hardware.

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Flight E5/712

Failed at Launch

- Signal Cable Pulled All the Way Out
- Many Feet of Tow Line Deployed (~30')
 - No Reel Counts Recorded

Problem Isolated to Cracked OPTO Coupler Chip on Reel Count CCA

- Examination Showed Ceramic Case Was Cracked Prior to Conformal Coating
 - Failure Mode Unique to This Circuit Card

Performed Detailed Inspection of Additional CCA's Pulled From Stock

- Evaluated 49 CCA's
- No Cracks Found

Corrective Action Initiated

- Additional Test Added Post ESS to Test OPTO Coupler Operation
- ✓ 100% Screening for All Mass Model and FOTD Rounds

Fallure Mode Identiffied - Corrective Action Implemented



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- Flight E5/714
- HVS Data Indicated Cathode Arcing While Climbing to 35K Feet
- Failure Mode Never Encountered in Prior Flight Test
- Canister, Decoy and Cable Were Extensively Tested To Re-Create/Identify the Failure
- Testing Conducted with High Voltage at Altitudes to 35K
- ⇒ No Evidence of Arcing Seen
- Conducted Evaluation of HVS Box (S/N 1) and Two Captive Carry Canisters (S/N 31 and 35) Used During Flight Testing
- Testing Conducted with High Voltage at Altitudes to 60K
- HVS Box and Canister S/N 31 Performance Normal
- Canister S/N 35 Exhibited Intermittent Arcing at 35K and Full Breakdown at 40K Feet
 - Further Inspection Revealed Damage to the Rubber Seal of the Vk Contact
 - ⇒ Connector Will Be Replaced Prior to FOTD AUR Flight
- Concluded That Recorded Cathode Failure Was Due to Captive Carry Canister S/N 31 and NOT TDM033

Evidence Indicates Flight E5/7/14 (7/1/2/02)। Fullly Successf



Flight E5/715

Decoy Separated During Maximum Performance Break Turn

- ~7 g's

Chase Reported Line Separation Immediately In Front of Decoy

- Confirmed With Post Flight Review of Chase Video
 - Confirmed When Line Was Returned

✓ Examination Showed Loose Areas and Tightly Wound Areas

Examination of Canister

- No Physical Evidence to Explain Loose Line at Deploy
- Pull Test Data Pre and Post Flight Indicated No Anomalies

Passed Same Maximum Performance Break Turn Several Times In Later Flights

No Additional Analysis Planned

Root Gause Unknown - No Corrective Action Planned





HVS Box Prematurely Started

- Did Not Capture HV Data for Last Hour of Flight

Canister, Decoy and Cable Were Extensively Tested and Evaluated

Testing Conducted with High Voltage at Altitudes to 35K

⇒ No Evidence of Arcing Seen

Physical Examination of the Returned Cable Showed No Evidence of Abnormal Wear or Twisting Seen in Other Failures Concluded That TDM035 Maintained Continuity Throughout Flight ndicates Filght E5/7/16 (7//22/02) Fully Successful



Flight E5/721

HV Cathode Short @ 35K, 5° AOA A/B Maneuver

Post Flight Review of Data Indicates Significant Thermal Stress to Line at 25K, 4 deg AOA A/B Maneuver

✓ Beyond Goal Envelope

Overstress Condition Resulted In Subsequent Short @ 35K

Tow/Signal Line Failure @ 5K, 3° AOA A/B Maneuver

Cathode Short @ 35K Resulted In 5 KV Arcing Throughout Remainder of Flight Recovered Cable Shows Evidence of Exposed Wires and Significant Arcing

Continuous Arcing Damaged Tow and Signal Jacket

Tow and Signal Line Ultimately Failed When Stressed During the 5K A/B Maneuver Evidence Indicates Flight E5/721 (8/14/02) Fall Exceeding Envelope Goal

Mass Model Rounds TDM018, 022, 024, 030 and 034

BAE SYSTEM

Flights F2/781 , E5/717

F2/782

2/783

E5/713

All Experienced Mechanical Failures Of The Signal Line

Detailed Analysis of the Units Revealed Several Similarities

All Had Good FO and Continuity From the Canister Through the Hot Zone 1

Indicates Failure Not Thermally Induced

- All Had Good FO and Continuity in the Canister
- S/N 18, 24 and 34 Had Good FO and Continuity in the Decoy
- ✓ Unable to Assess S/N 22 and 30 Since The Units Sustained Mechanical Damage to the Termination at Landing
 - All Showed Area of High Twisting Past the Hot Zone
- Preliminary Failure Mode Attributed to Heavy Twisting Of The Signal

Faffure Mode Identiffed - Further Analysis Required

EXHIBIT "C"

BAE SYSTEMS

Post Flight Tow/Signal Line Analysis

Dr. J. Dion





Post Flight Cable Analysis Process

Line Layout Inspection Process

- Untangle
- LayoutOptical Inspection (to 50X)
 - Digital Photos

Continuity Evaluation

Electrical & Fiber

High Pot Testing

- Standard Temperature and Pressure
- Altitude Chamber



TDM033 Assessment

BAE SYSTEMS

 A/B Maneuvers •Flight E5/714 Mission Data •7/12/02 · FO continuous from decoy Electric continuity throughout (no shorts) No Arcing on egress hole 100 ft. Tap point No HV shorts throughout Towline survived flight test points • Recoil / Landing / Handling FO Break(s) from: • FO continuous from canister 100 ft. Tap point Mild "goal post" wear ~11.12 feet ~ 0.5 ends cut at 2.5" ~8.5" from cut end ~ 1-2 ends abraded High Potted...wires visually examined. No Arc spots on Flapper damage from cut end No HV Shorts on the spool Canister Spool

Visual of Decoy and spool line for arcing, negative

No A/B heat induced damage visible

Zylon Color Normal

Minor "Pooching"

Representative of Fully Successfull Flight

BAE SYSTEMS Information & Electronic Systems Integration, Inc. **BAE SYSTEMS Proprietary Information**



TDM035 Assessment

 Combat Maneuvers Mission Data Flight E5/716 •7/22/02

A/B Maneuvers No Arcing on egress hole FO continuous from canister Recoil / Landing / Handling 116 ft. Tap point Towline apparently survived flight test FO Break(s) from: Zylon braid deformation into Uncoiled Signal from Tow PEEK & EKJ -20-24ft from Can "Hot Zone" < ~4ft > Mild "goal post" wear ~11-12 feet Canister

Electric continuity throughout (no shorts)

No HV shorts throughout

Small Peek/Braid extrusion

Possible PEEK melting

PEEK softened

No A/B heat induced damage visible

Zylon Color little darker in 'Hot Zone'

Minor "Pooching"

Flapper damage (Tow & Signal)

~5" from cut end

~ 1.2 ends abraded (both) & cut on tow

~ 0.5" ends cut at 2.5" from cut end on tow

& abraded on both

Representative of Fully Successful Flight

BAE SYSTEMS Information & Electronic Systems Integration, Inc. **BAE SYSTEMS Proprietary Information**



TDM030 Assessment

AE SYSTEMS

* Passed 5k 3° AOA A/B; Fiber Optic failed during 2° AOA A/B, HV passed 3, 2, 1 AOA

 Combat Maneuvers A/B Maneuvers **Mission Data** Flight E5/713 **Decoy Sustained** Damage During •7/11/02 Landing FIBER Gore's "wire" pitch increased Severe Signal line pitch/twist JANANANANANA **PEEK Distortion** (fiber failure region) 35-55 ft from decoy Kinking heavily • #Fiber Optic continuous 100-ft. tap point from can Zylon braid deformation into Uncoiled Signal from Tow Possible PEEK melting PEEK softened PEEK & EKJ ~52.60 ft from canister: Discoloration of Tow & Signal ~ 0.5 ends cut at 2.5" from cut Minor abrasion ~40-90 ft. from canister: ~8.5" from cut end, ~ 1-2 ends abraded Pooching Flapper damage Canister

~11-12 feet Mild "goal post" wear

Light Abrasion of Signal Line Through-out

FAILURE

Zylon Color Normal

No heat induced damage visible

Electric continuity throughout (No Shorting)

Heavy Twist Failure

Representative o



Cable Inspection Summary

POST FLIGHT CONDITIONS	Comments	Probable failure mode: High twisting on signal line.	Probable failure mode: High twisting on signal line. Survived MIL Power testing to ~30° AOA. 2 wear areas seen.	Probable failure mode: High twisting on signal line. Very short flight. Signal line wear pattern offset at stand-off.	NA	Probable failure mode: High twisting on signal line.	No shorts @ 5kV throughout Note: Line "pristine"	Probable failure mode: Looseness of Line and Twisting	No shorts @ 5kV throughout. HVS Data logger off during A/B	Probable failure mode: High twisting on signal line.	25k A/B 4° test pt. damaged the EKJ, resulting in 35k A/B failure. 5 kV arcing damage weakened line resulting in line breakage
POST FI	"Hot Zone" Electrical	Continuity No shorts @ 5kV	Continuity No shorts @ 5kV	Continuity No shorts @ 5kV	NA	Continuity No shorts	Continuity No shorts @ 5kV	Continuity No shorts	Continuity No shorts @ 5kV	Continuity No shorts	Continuity No shorts to 30 ft.
	"Hot Zone" Fiber	Continuity	Continuity	Continuity	NA	Continuity	Continuity	Continuity	Continuity	Continuity	Continuity to 30 ft.
	Electric Continuity	Yes	lost prior to 5k A/B	lost @ 5k A/B	NA	Yes	Yes	Lost Decoy	Most Likely	Lost @ 45° dive	HV high @ 25k A/B HV lost @ 35k A/B
CONDITIONS	F.O. Continuity	Lost @ 5k A/B	Lost prior to 5k A/B	Lost @ 5k A/B	NA	Lost @ 5k AB	Yes	Lost Decoy	Yes	Lost @ 45° dive	Lost @ 5k A/B
IN FLIGHT CO	Plume A / B	Yes	N _o	Yes	NA	Yes	Yes	oN N	Yes	No	Yes
	Snubber	G.R.	G.R.	G.R.	NA	BAE	BAE	BAE	BAE	BAE	BAE
	Flight	TDM018	TDM022	TDM024	TDM017	TDM030	TDM033	TDM029	TDM035	TDM034	TDM028



Cable Guide Damage Summary

Cable Guide

- Rubber Worn Through to Metal All Flights
- ✓ Wear Patch Positioned the Same on All Flights
- ⇒ Typical Damage (No Electrical / Optical Problems)
- ⇒ Off Center to the Left Looking Out Though the Rear Can

Lines @ Cable Guide

- Tow: Some Fiber Ends Cut Though Due to Flapper
- ✓ Damage Occurs on 1 Side (All Flights)
- ⇒ Implies No Twisting/Rolling
- Signal: Fibers Frayed at Varying Degrees
- Conductors and FO Kinked Slightly

Cable Guide Wear Normal

Goal Post Damage Summary



Light Abrasion on Cable

No Broken Fiber Ends

Signal Line Jacket

Very Light Abrasion

2 Visible Wear Areas on TDM022 (Greene Rubber Snubber)

Wear Pattern Offset on TDM024 (Greene Rubber Snubber)

- 1 Consistent Wear Area On All BAE Snubber

✓ No Evidence of Excess Signal Line

Post Wear Normal/BAE Snubber Provides



Plume Survivability Highlights

Max A/B

- F.O. Continuity Maintained Throughout Hot Section
- 4 Mil EKJ Leakage Seen at Various Test Points
- ✓ All Leakage Within Goal Envelope Recoverable
- Post Flight Analysis (Continuity, HV & Microscopy) Shows No Permanent Degradation in EKJ, F.O./ Coatings
- ✓ Polyimide Buffer Pristine

MIL Power

F.O. Continuity & No Leakage at All Mil Power Test Points

✓ to 30° AOA





High Twist Mechanical Failure Theory

BAE SYSTEMS

Failure Mode: Signal Line Slip Over the Tow Line

Effects

Signal Line Slip Results In Regions of High Twist

Twisting (Torsion Stress) Adds to the Tensile Stresses and Eventually Dominates

⇒ FO More Sensitive to Twisting

⇒ Local EKJ Thinning Can Create HV Arcs

Signal Line Slip Can Also Form Regions of Line Separation

Root Cause/Corrective Action Has Not Been Determined

Further Analysis/Testing Required

B. Sarantis

Conclusions and Recommendations





Conclusions

System Performance Exceeded Thermal Expectations for Phase C

· F.O. Survives Thermal Plume Conditions Tested

✓ Fiber More Robust Than Dielectric

4 Mil EKJ Survives Thermal Plume Conditions Tested Within Goal Envelope

Signal Line Jacket Hot Section Good From Plume Perspective

✓ 6K Denier through 1st 100′

- Towline More Than Adequate

Signal Line Slip Improved With BAE Snubber

Mechanical Failures Due to Heavy Twisting of Line

- FO Breaks

- Opens / Arcing

- Line Fracture &/or Decoy Separation

Separation Performance Marginal

Surface Scratches > 350 KCAS

No Damage to Mass Model Decoy



Recommendations

Proceed to Envelope Expansion Testing

- Determine Root Cause and Corrective Action for Observed Local **Line Twisting**
- Develop an Analytical Understanding and Augment With Experiments
- Laboratory Testing Will Supplement Analysis to Promote Better Understanding of Phenomena
- Experiments Will Be Designed Specifically to Address Flight Observations and Analysis Results
- ⇒ Further Dedicated Corrective Action Testing Will Be Performed
- Sufficient Funds Remain To Accomplish Root Cause Investigation
- ✓ Contract Extension Required
- Incorporate Corrective Action In Future Product Improvements

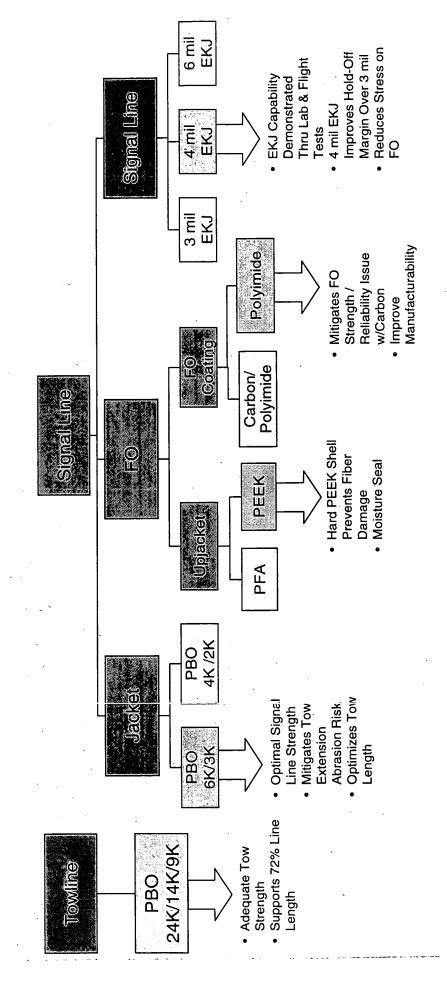
Back-Up







Downselected Tow/Signal Line Configuration BAE SYSTEMS



Supports 58% Deployment Length

Brake Control Response Reference

Blue - DAC, a measure of current supplied to the brake. Red - Acceleration profile of spool during deployment High DAC=low brake force and vice versa Mar 28 2001 20kft, 250 KCAS F/18 Slot 3, 3109000G5 SN60 0 = Maximum brake force Magenta - Actual deployment velocity 2000 Black - Desired deployment velocity • 264 = No brake force Curve definitions are as follows: 1500 - DAG-

BAE SYSTEMS Proprietary Information BAE SYSTEMS Information & Electronic Systems Integration, Inc.



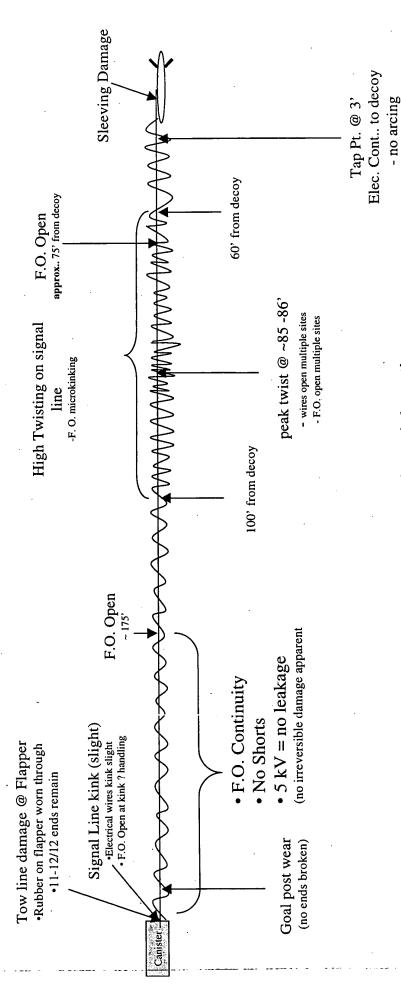
TDM018 Assessment

BAESYSTEM



Total Time:

- F.O. open: 54 min.
- 350Vopen: 59 min.
- Intermittent shorts: 59 + min.
- Flight duration: 64 min.



BAE SYSTEMS Proprietary Information BAE SYSTEMS Information & Electronic Systems Integration, Inc.



FDM022 Assessment

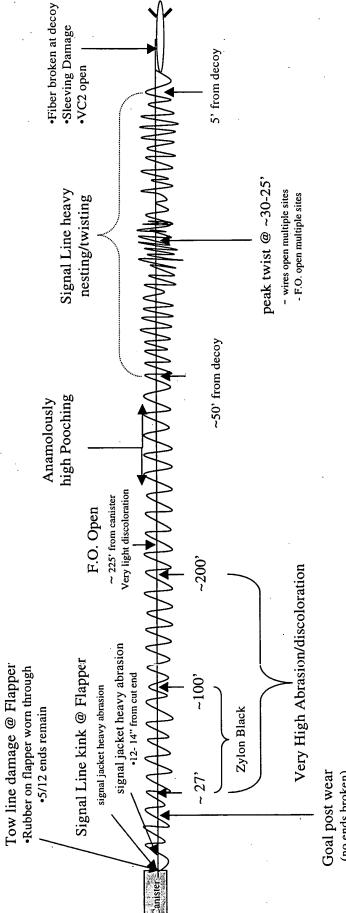
FO lost @: 5kft setting up for 1st A/B test pt. Survived Mil Power testing to very high AOA

Total Time:

• F.O. open: 96 min.

• Vk short to 350: 98min.

• Flight duration: 109 min.

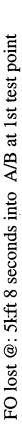


·Light abrasion on Tow (no ends broken)

·light abrasion on Signal line 2 places

BAE SYSTEMS Information & Electronic Systems Integration, Inc. **BAE SYSTEMS Proprietary Information**

TDM024 Assessment



Tow line damage @ Flapper

Total Time:

•F.O. open: 2.5 min. •350Vopen: 2.6min.

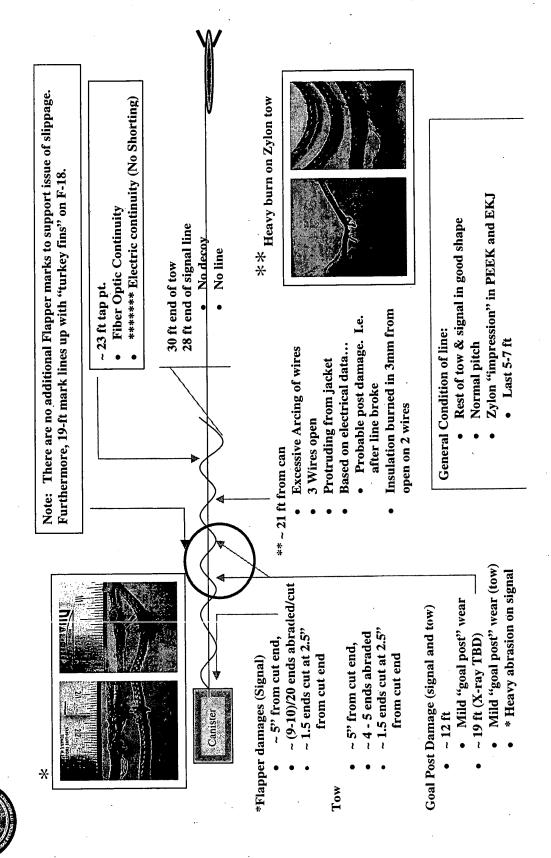
min. •Flight duration::47

Sleeving Damage F.O. Open ~50' from decoy Elec. Cont. to decoy - no arcing Tap Pt. @ 3' ~ 40 ' from decoy peak twist @ ~50-52" wires open multiple sites
 F.O. open multiple sites Heavy nesting/twisting - 4 wires open - F.O. open ~70 ' from decoy 1 wire continuous (no visible Damage) F.O. open ~ 235' from canister F.O. open ~ 6" before goal Post F.O. open ~ 22' from canister (pop-out) kink (slight) @ flapper •Rubber on flapper worn through Signal Line / wires •10-11/12 ends remain (no visible damage) F.O. open ~ 17' from canister Goal post wear (no ends broken)

•Center of wear areas offset 3-4" verylight abrasion on Signal Light abrasion on Tow

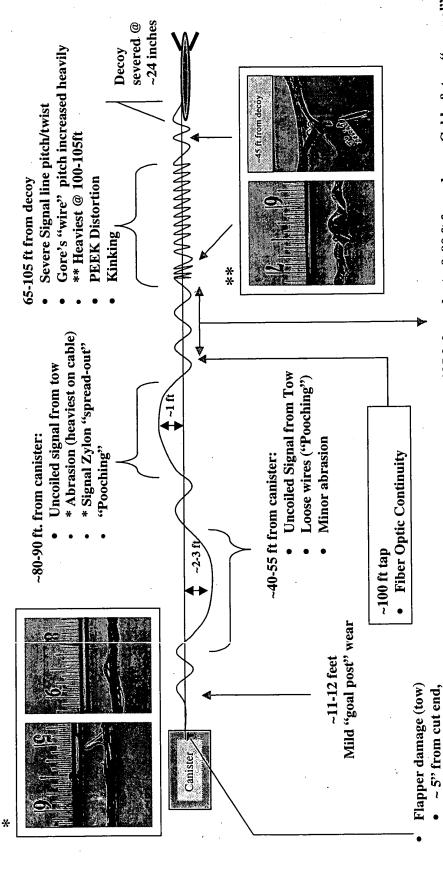
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TDM028 Assessment



BAE SYSTEMS Proprietary Information
BAE SYSTEMS Information & Electronic Systems Integration, Inc.

TDM034 Assessment



Between 105 ft from decoy & 90 ft from decoy, Cable & tow "normal"

- Light Abrasion of Signal Line Through-out
 - Zylon Color Normal

***** Electric continuity throughout (No Shorting)

handling / snapback..."

details lost due to

Signal jacket mild wear

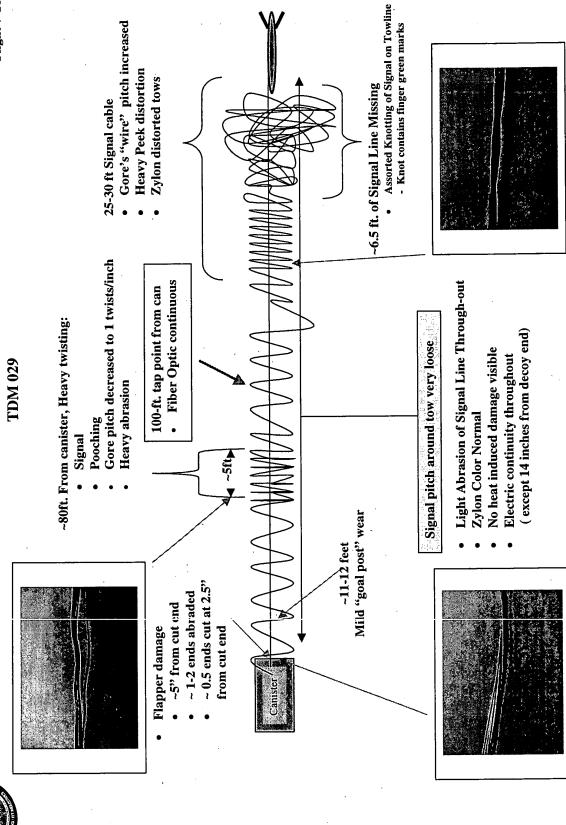
~ 4 - 5 ends abraded ~ 1.5 ends cut at 2.5"

from cut end



TDM029 Assessment





BAE SYSTEMS Information & Electronic Systems Integration, Inc. **BAE SYSTEMS Proprietary Information**

High Twist Failure Action Plan

BAESYSTEMS

- Re-look at Flight Test Data Using Parameter Fusion to Perform Trend Analysis
- Merge Calculated System States for Flight Conditions of Interest
- ✓ Includes: Tension, Droop, Decoy AOA, Fin Sweep, Etc.
- ⇒ Data Feeds Subsequent Actions
- Analyze Flight Conditions Where Anomalies Occur
- Calculate Line Vibration Frequencies and Amplitudes
- Design Experiments to Emulate Flight Conditions / Results.
- Vary Key Round Parameters, E.G., Snubber Back Tension, Cable Capstan Effect, Etc.
- ✓ Experiment Will Be Utilized to Assess Relative Merit of Corrective Actions
 - Utilize Existing Modeling Capability, 6 DOF, and Current Laboratory Facilities. Conduct Modified Experiment, Similar to B-1B Fixture, Will Be Utilized to
- Develop Solution to Problem Within Framework of Existing Variable Set

Assess Improvements

- Example: Increase Snubber Back Tension, Modify Tow Cable Coating Locally to Improve Adhesion, Modify Signal Cable Elements to Change Stiffness Memory, Etc.
- Validate Relative Change to System Performance Using Experiment Previously Designed

BAE SYSTEMS Proprietary Information BAE SYSTEMS Information & Electronic Systems Integration, Inc.

Selected Configuration - Towline Upgrade

0.072" @ 24k Denier

0.052" @ 12K Denier 0.040" @ 9K Denier



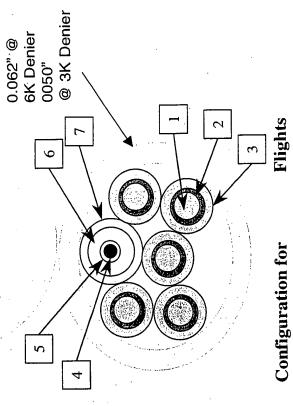
-	
Baseline	Upgrade
2 Stage	3 Stage
	24k / 12k / 9k
12k / 9k denier	denier
Signal	Signal - Jacket
Baseline	Upgrade
2k denier	6k / 3k denier

	Signal - Co	Conductors
	Baseline	Upgrade
1	32 Ga copper	32 Ga copper
	MIL-ENE	PTFE
Q	0.002" / 0.003"	0.0005"
		CXE
3	N/A	0.004"

0.045"

	Signal - Optics	Optics
	Baseline	Upgrade
4	Glass	Glass
	Acrylate	Polyimide
S	245 microns	152 microns
	PTFE	PTFE
9	0.003"	0.003"
	FEP	PEEK
7	600 micron OD	600 micron OD

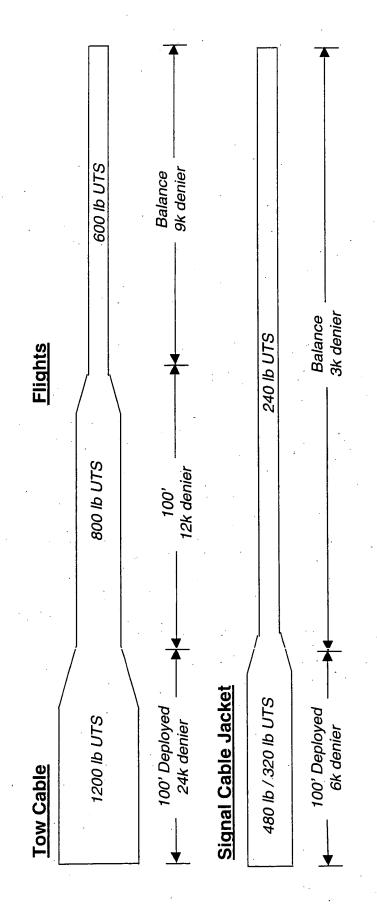
Baseline Cable System







Selected Configuration - Towline Upgrade



- Packaged length
- Tow 72% spec
- Signal 61% spec
- Deploy Length = 58% spec
- Worst Case Margin (@58% spec)

- Tow: 3.3 Signal: 3.6 Glass better than 200%

Future Optimization Paths





Length Optimization Areas

Redesign Canister to Optimize cable

- Repartition signal and tow spindle sizes

Bounded by other canister constraints

Optimize Tow Cable Diameter

Change Insulation Material

Reduce Fiber Optic Coatings

Install Moisture Barrier

- May allow thinning of insulation

Rerouting of 350V and ground to tow cable



Anomolous Leakage Current

There is a general relationship between leakage and high temp

Leakage ~ exp (T)

Phase A testing showed ~ mA's of leakage through the dielectric

Lab testing at expected temperatures results in µA of leakage

Potential reasons for the discrepancy

- Temperature incorrect

Length effect

- Environment

Water

Free Radicals

UV Photons



Lab Testing EKJ Insulation

Leakage linear with length

Water however produced a significant increase in leakage and a decrease in breakdown strength Free Radicals and/or UV Photons could also reduce breakdown strength

Water effect also consistent with NRL's data

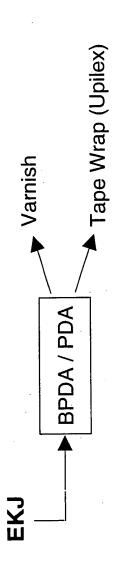
Potential Solution:

Add plume gas barrier by wrapping metalized film between the Zylon jacket and the wires/fiber optic section

If NRL's temperatures are true, a plume gas barrier will allow for reduced wire insulation thickness



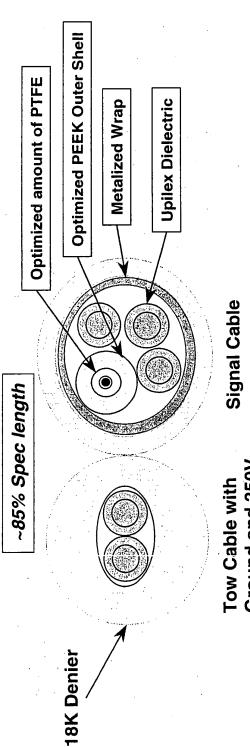
Dielectric Roadmap



- "Upilex-S" varnish at 1-3 mils (recently coated on a 36 Ga wire)
- 1 mil of "Upilex-S" varnish is equivalent to ~ 3 mils of EKJ
 - 5kV up to ~450C
- "Upilex-S" varnish also being developed through Navy SBIR contract with local companies



Potential Concept to Grow Length/AB AOA



Ground and 350V

Tow line braid has dead space

 Adding two conductors/36-34 AWG reduction allows no/limited diameter growth

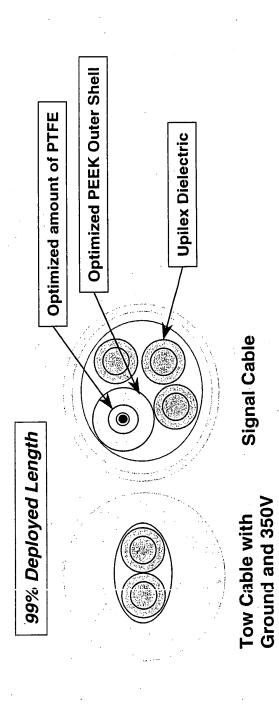
Added benefit increases plume exposure

- 5kV difference is now dissipated over 0.020" to 0.030"
- Signal jacket 2.5kV

Lab testing exceeds ALE-50 performance. Breakdown 0.003" EKJ increased to 550C



Potential Concept to Grow Baseline Length



- Tow line braid has dead space
- Adding two conductors/36-34 AWG reduction allows no/limited diameter growth
- Signal jacket diameter reduced from 0.045" ightarrow 0.032"
- Drag loads reduced

Signal jacket 2.5kV allows insulation reduction

Estimated deployable length 1 from 90% to 99% with canister repartitioning



Summary

Substantial improvements made to the tow/signal cable endurance

- Survived 200 seconds of A/B exposure

Flight testing of selected configuration

Further Improvements being investigated

- Improve line length and thermal endurance



Dielectric (Conductor Insulation) Downselect

High performance Polymer Dielectrics

- Upilex-S is considered to be the best high temperature polymer film
- Film is not manufactured with an adhesive for insulation wrapping
- Upilex-S as a "varnish" is not yet "commercially" available
- Kapton H with FEP adhesive is a common high temperature insulation (rated to 260C)
- Properties not a good as Upilex-S
- 'Mixing' Kapton H & Upilex-S is next best polymer film commercially available as Kapton E (new material)
- Can be made with type KJ adhesive
- Better performance than FEP or PFA adhesives
- Material referred to as EKJ

Driven by Original RFCM IB3 OPEVAL Schedule U Insulation Selected as Candidate

.....

Up jacket



FO Coating (Buffer/Upjack_t) Candidates and Downselect

Options Considered

- Buffer

Carbon/Polyimide

Polyimide

Metalization/Polyimide

Upjacket

PFA (high temperature replacement for FEP)

PEEK (vendors could not support for Phase A testing)

Candidates Selected

Buffer: Carbon/Polyimide or Polyimide

Upjacket: PFA or PEFK

• All Options Support 500°C Operation in the Lab

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Towline and Signal Line Jacket **Candidates and Downselect**

Options Considered

- Silicon Carbide
- CarbonCobalt Nickel Superalloy
 - Various Others

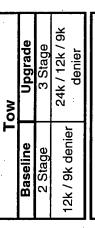
Options Tested

- Silicon Carbide
- Carbon
- Zylon

Zylon Selected as Candidate Material

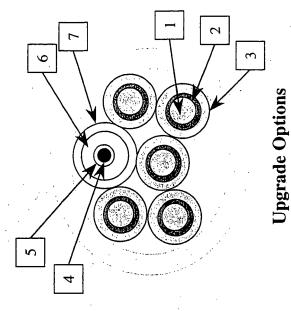
• Best Strength-to-Weight Ratio @ 500°C

Cable System Flight Test Configurations



Signal	- Jacket
Baseline	Upgrade
2k denier	9k / 3k denier 4k / 2k denier

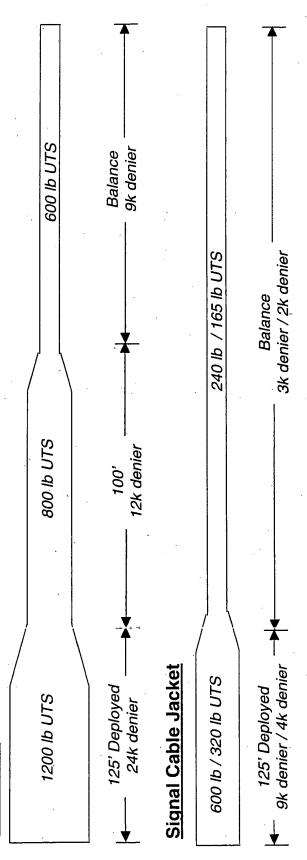
BaselineUpgrade4GlassGlass5AcrylatePolyimide6245 microns152 microns6PTFEPTFE0.003"0.003"7FEPPFA and PEEK600 micron OD600 micron OD		Signal - Optics	Optics
Glass Acrylate 245 microns PTFE 0.003" FEP 600 micron OD		Baseline	Upgrade
Acrylate 245 microns PTFE 0.003" FEP 600 micron OD	4	Glass	Glass
245 microns PTFE 0.003" FEP 600 micron OD	Ľ	Acrylate	Polyimide
PTFE 0.003" FEP 600 micron OD	2	245 microns	152 microns
0.003" FEP 600 micron OD	Ú	DTFE.	PTFE
	0	0.003"	0.003"
	1	FEP	PFA and PEEK
		600 micron OD	600 micron OD





Cable System Flight Test Configurations

Tow Cable



Configuration	Tow	Signal Jacket	HV Insulation FO Coating	FO Coating	FO Upjacket	Deploy Length
,G1	24K/12/9K	9K/3K	3 mil EKJ	Carbon	PFA	64%
,G2	24K/12/9K	9K/3K	4 mil EKJ	No Carbon	PEEK	48%
,G3	24K/12/9K	4K/2K	6 mil EKJ	Carbon	PFA	20%
,G4	24K/12/9K	9K/3K	4 mil EKJ	Carbon	PFA	29%
,G5	24K/12/9K	9K/3K	4 mil EKJ	No Carbon	PFA	29%



Flight Test Considerations

Known Issues Entering Tests

- Carbon coating on glass reduces strength
- Significant handling problems during assembly (BAE SYSTEMS and GORE)
- 1 unit wired to show good continuity due to fiber breakage
- Expected poor optical performance from carbon configuration prior to testing
- 0.006" EKJ puts additional stress on the PFA upjacketed fiber

F/A-18E/F Towline Durability Flight Test Results

		Total H V Flectrical			AOA	AOA Achiev d	d
Configuration	Flights	Continuity	Total Optical Time	Total A/B Time	5 kft	15 kft	35 kft
0.003" EKJ Insulation Carbon/PFA Upjacket Launch Condition: 336 psf	4	368 minutes	Two successful flights totaling 197 minutes (1 hard wired good 1 failure at launch)	906 seconds	င်း	ဗိ	7°
0.006" EKJ Insulation Carbon/PFA Upjacket Launch Condition: 336 psf	2	20 minutes (Test box off on one test)	3 seconds (Both lost during launch)	274 seconds	5°	င်း	7°
0.004" EKJ insulation No Carbon/PEEK Upjacket Launch Condition: 700 psf	CV .	36 minutes (Test box off on one test)	78 minutes (Both good to end of flight Cable damaged on Camera)	37 seconds (one flight done only with MIL power)	N/A	N/A	7°



Flight Test Results

No instances of tow line burnoff

- Minimal damage seen

0.003" EKJ successfully passed all AOA conditions tested

0.006" EKJ met 2 of 3 AOA conditions (4K denier jacket failed)

0.004" EKJ met test conditions @ 35 kft (not tested at 5 kft or 15 kft)

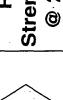
Carbon/PFA

- 3 of 5 failed at launch

2 survived until test was terminated

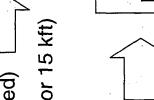
Non-carbon/PEEK

2 flights at higher Launch Qs survived until test was terminated



Positive
Strength Margin
@ 24K Zylon

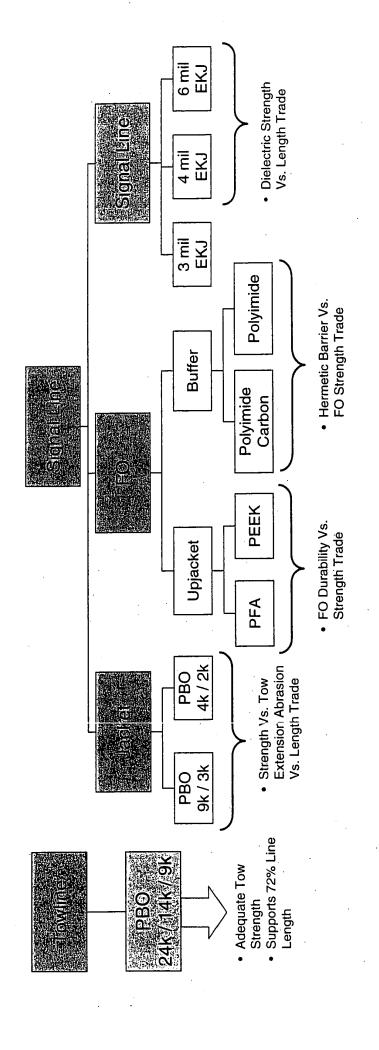
Positive Results w/EKJ



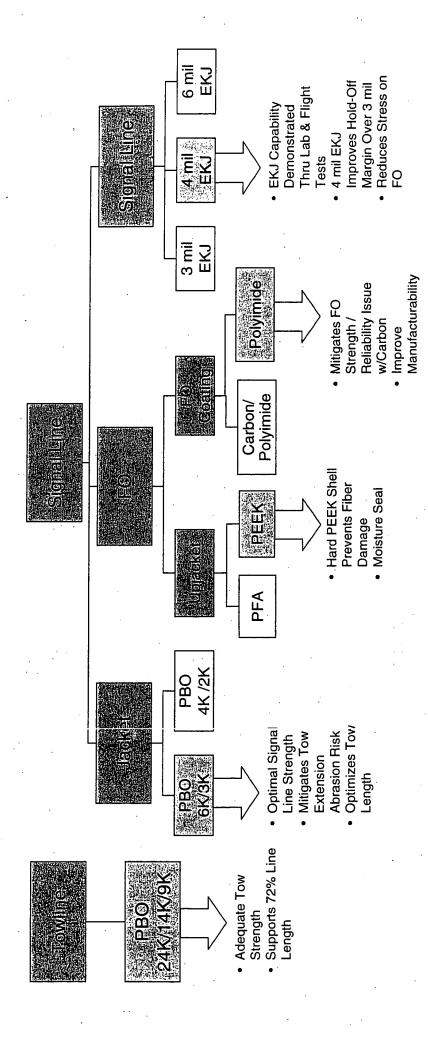
FO Performance Marginal w/Carbon

Cable Options Summary

)



Downselected Configuration for Towline Upgrade (F/A-18E/F)



Supports 58% Deployment Length



PEEK vs. PFA Upjacket Trade

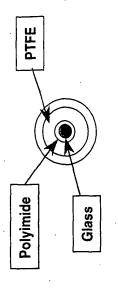
Flight data shows local damage, occurring during deployment, causes the highest stress

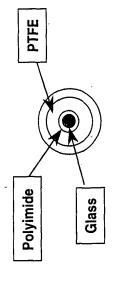
PFA allows greater length

- PFA (Like FEP) cold flows
- Mechanical deformation seen on
- ✓ Wound spindles
- / Deployed signal line

Hard PEEK provides resistance to winding/deployment

- No damage seen post wind/deployment
- Recovered field hardware shows no upjacket deformation
- Field return still continuous

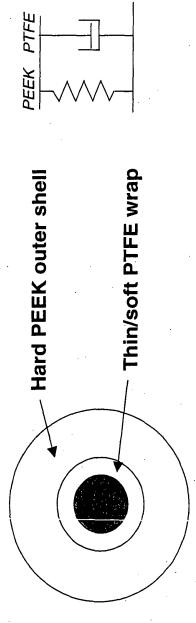






PEEK/PTFE/FO Construction

The stiff PEEK shell provides crushing protection during winding/storage/deployment



The soft PTFE layer allows the fragile glass to 'float' within the **PEEK shell**

- Absorbs energy during deployment
- Reduced thermal shock during plume exposure

Coating thickness reduction very possible to improve line length

PEEK and PTFE also protect the glass fiber from water